Yellowjacket Joint Venture
Suite 200, 16 - 11th Ave. S.
Cranbrook, BC
V1C 2P1

Mr. Loren Kelly
Chair NWMDRC

Re: Yellowjacket Gold Mine Project – Effluent Quality

During the scoping review of the small *Mines Act* Permit Application – Yellowjacket Gold Mine Project it was indicated by MEMPR that there was a general concern with ML/ARD potential of the mineralized material, which would invariability effect the effluent (tailings slurry) discharge quality of the process plant.

The Lorax Environmental work in 2007 on the bulk sample materials was reported in the document entitled "*Yellowjacket Property Bulk Sample Waste Characterization Program, March 2009",* which is (Appendix 3 – Small *Mines Act* Permit Application) at www.yellowjacketgold.com. The document indicated that there were no ARD concerns; however a potential neutral metal leaching concern due to the (ultramafic) lithology of the deposit was indicated as a conclusion. As the non-economic waste material is being backfilled into the mined out pit and eventually flooded the metal leaching from this material was less of an issue. However, the mineralized materials that will be put through the process plant and eventually end up in the tailings storage facility (TSF) would need to be evaluated. Unfortunately, at the time of submission of both the small *Mines Act* and Effluent Permit Applications the company did not have any tailings solids or supernant quality results to assess or report.

Tailings solids were collected in March 2009 and submitted for size fraction analysis, modified ABA (total sulphur, etc.) and low level metals by aqua regia digestion with ICP-NS Finish. Solid-phase metal analysis was not conducted on the tailings samples due to the fact that they are tailings that have been crushed, ground, washed and deposited sub-aqueous. Results of the completed analysis were recently received and indicate that the tailings are 95 to 99% passing #200 mesh, and that the ABA and metal analysis indicate that the tailings look very similar to the results obtained from the bulk sample characterization: High Neutralizing Potential, Low Acid Potential and metals concentrations suggesting that the bulk of the material is serpentine/ultramafic lithologies. Although, the metal elements present are in high concentrations, it does necessarily mean that they will be present in high concentrations in tailings and/or waste rock effluent, due to the mineralogical associations of this metals as well as the chemistry of the infiltrating waters. Information regarding the results of the recent tailing sample analysis is attached to this summary.

As part of the monitoring program proposed by the Yellowjacket JV, tailings supernant will be sampled and an assessment of the potential water quality impacts determined prior to completion of the current bulk sample processing.

In the meantime, to assist in alleviating the potential concerns in the absence of project tailings slurry qualities, the Yellowjacket JV had Lorax develop a preliminary impact assessment of the project's tailings effluent using their knowledge of the Ekati Project, which has very similar lithologies. Lorax produced a technical memorandum entitled *"Preliminary Impact Assessment of Yellowjacket Process Plant discharge on Pine Creek Water Quality". April 27, 2009"*, which is attached to this summary.

The objective of the technical memorandum was to provide a preliminary evaluation of the potential impacts to Pine Creek water quality resulting from the discharge of the Yellowjacket process plant supernatant.

To evaluate the impact of the process plant discharge on the chemistry of Pine Creek, reasonable estimates of water quantity and quality were required. The following Table 1 - Yellowjacket Process Plant and Pine Creek Flow Rates provides a summary of the maximum flow rates expected from the Yellowjacket process plant, as well as the flow conditions within Pine Creek including low flow, average flow, and high flow. For the purposes of conducting a preliminary assessment of the impacts of Yellowjacket process plant discharge on Pine Creek water quality, it has been assumed that all effluent water from the process plant will discharge directly into Pine Creek. Based on this assumption, dilution factors, which have been calculated by dividing Pine Creek flow rates by the process plant discharge flow rate, are also reported in Table 1. These values demonstrate that even at winter low flow conditions, process plant effluent discharged directly to Pine Creek will be diluted at a minimum of approximately 250 times. However, it is important to note that the low flow value included in Table 1 is from winter, when discharge from the process plant is not expected. Therefore, average and high flow dilution values provide a more reasonable estimation of the dilution expected within Pine Creek. While there is a good understanding of the quantity of water flowing from the process plant and within Pine Creek, there is currently no Knelson process plant water quality or kinetic leach experiment data currently available from the Yellowjacket Project, in order to evaluate the quality of process plant discharge. Therefore, in the absence of site specific data, a reasonable approximation of Yellowjacket process plant discharge water chemistry was required and this is the Ekati Mine.

Table 1:
Yellowjacket Process Plant and Pine Creek Flow Rates.

Source	Flow	Dilution Factor
Process Plant Discharge	0.0056 m^3/s	250
	Low: 1.4 m^3/s	750
Pine Creek Flow[1]	Average:4.2 m^3/s	2500
	High:14 m^3/s	

[1] Pine Creek Flow values from Sigma (2006)

Ekati kimberlite is a mantle derived ultramafic volcanic rock that is composed predominantly of olivine and serpentine, both of which are common constituents of the mafic and ultramafic lithologies that dominate the Atlin Ophiolitic Complex where the Yellowjacket Property is located. Kimberlite ore at Ekati is processed by crushing, washing, and gravity separation without the use of additional chemicals, very similar to the processing scheme that will be employed at Yellowjacket. It has been estimated that approximately 13,000 tonnes to 16,000 tonnes of ore are processed daily at Ekati (Day et al. 2003) using approximately 9,000 m^3 to 16,000 m^3 of water (Lee 2005), which produces water-rock ratios ranging from 0.7 m^3 water/ tonne up to 1 m^3 water/ tonne. The geology, ore processing scheme and process plant water-rock ratios at Ekati are similar to those expected from the Yellowjacket project. Therefore, process plant discharge water quality from Ekati may serve as a reasonable approximation of process plant discharge expected from the Yellowjacket project.

Table 2 provides a summary of average process plant discharge water chemistry collected from Ekati between 2000 and 2002 (Rollo and Jamieson 2006). Note that only parameters with associated BC water quality objectives have been included in this analysis. This table also contains diluted Ekati process plant discharge concentrations, calculated by dividing the average process plant concentrations listed in Table 2 by the dilution factors listed in Table 1. Additionally, the detection limits that are currently being used for the 2009 Yellowjacket water quality monitoring program are included in this table for comparative purposes. For ease of comparison, the diluted concentrations reported in Table 2 have been formatted to the same number of decimal places as the detection limits. While these data demonstrate that the majority of trace metal concentrations in diluted process plant discharge waters are at or below the detection limits used in the 2009 water quality monitoring program, molybdenum and nickel are indicated to be present in detectable concentrations in diluted waters. However, comparison with baseline water quality data from Pine Creek demonstrates that the predicted concentrations for these parameters are at least an order of magnitude lower than the minimum baseline values.

As mentioned previously, Yellowjacket process plant effluent will not be discharged directly into Pine Creek; rather, it will be allowed to exfiltrate through the alluvial gravels of the Pine Creek floodplain. As a result of metal attenuation mechanisms within the alluvial gravel groundwater system, concentrations entering Pine Creek will most likely be less than those expected directly from the process plant. Therefore, these calculations, which provide a conservative overestimate of the potential impacts to Pine Creek, suggest that the discharge of Yellowjacket Process Plant effluent directly into Pine Creek will not have a significant impact on water quality

Table 2:

Average Process Plant Discharge water chemistry from Ekati Diamond Mine and Associated Dilution Calculations. Only parameters with BC water quality objectives have been included in this table. All values reported as mg/L unless specified otherwise.

		Diluted Concentration			
	Average[1]	**Low Flow[2]**	**Average Flow[3]**	**High Flow[4]**	**2009 Detection Limit**
SO4	212	0.8	0.3	0.1	0.5
Cl	30.8	0.1	0.0	0.0	0.5
F	0.076	0.00	0.00	0.00	0.01
Ag	0.0002	0.000001	0.000000	0.000000	0.000005
Al	0.001	0.0000	0.0000	0.0000	0.0002
As	0.0126	0.00005	0.00002	0.00001	0.00002
B	0.0528	0.00	0.00	0.00	0.05
Cd	0.00066	0.000003	0.000001	0.000000	0.000005
Co	0.00051	0.000002	0.000001	0.000000	0.000005
Cr	0.00258	0.0000	0.0000	0.0000	0.0001
Cu	0.00156	0.00001	0.00000	0.00000	0.00005
Fe	0.046	0.000	0.000	0.000	0.001
Mn	0.0161	0.00006	0.00002	0.00001	0.00005
Mo	0.409	0.00164	0.00049	0.00016	0.00005
Ni	0.055	0.00022	0.00007	0.00002	0.00002
Pb	0.00006	0.000000	0.000000	0.000000	0.000005
Sb	0.02793	0.00011	0.00003	0.00001	0.00002
Se	0.00258	0.00001	0.00000	0.00000	0.00004
U	0.0002	0.000001	0.000000	0.000000	0.000002
V	0.0039	0.0000	0.0000	0.0000	0.0002
Zn	0.0042	0.0000	0.0000	0.0000	0.0001
1 Data from Rollo and Jamieson (2006)					
2 Dilution factor = 250 (Table 1)					
3 Dilution factor = 750 (Table 1)					
4 Dilution factor = 2500 (Table 1)					
5 Reported as mg CaCO3/L					

Regards,

Charles "Chuck" Downie
Yellowjacket Joint Venture

Attachments: a.) Tailings Analysis Results, May 2009
b.) *Preliminary Impact Assessment of Yellowjacket Process Plant discharge on Pine Creek Water Quality". April 27, 2009*

Golder Associates Ltd. - Burnaby Laboratory
4280 Still Creek Drive
Burnaby, B.C. Canada V5C 6C6

PARTICLE SIZE ANALYSIS OF SOILS

Reference
ASTM D 422-63 (2007)

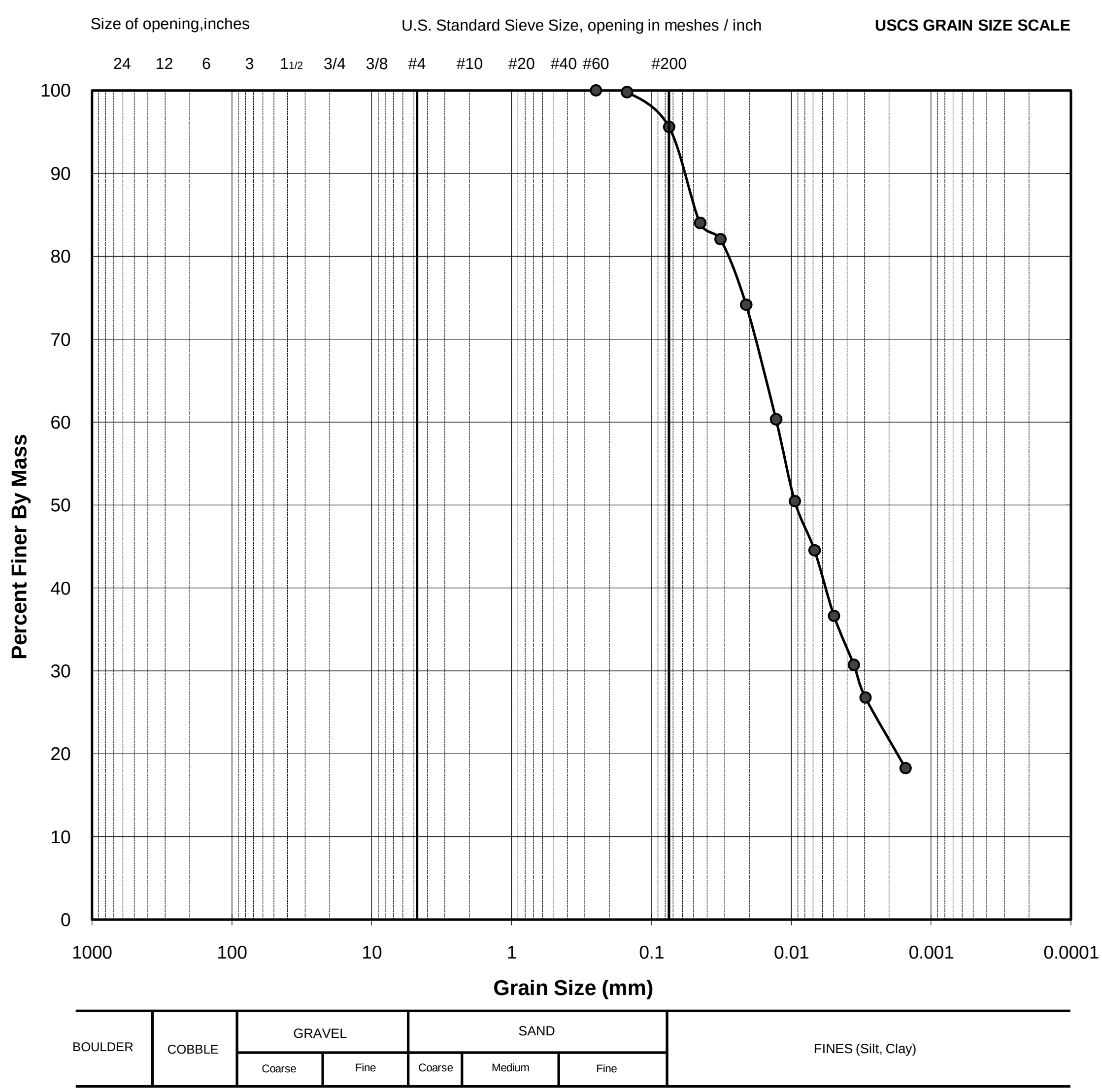
Project No.:	07-1416-0140	**Sample:**	**T1**
Client:	SGS Cemi Inc.	**Borehole No.:**	N/A
Project:	#0640	**Depth (m):**	N/A
Location:	Prize Mining Corp.	**Lab ID No:**	052

Specific Gravity (assumed): 2.70

Other Remarks:

Dispersion Method: Stirring
Dispersion Period (min): N/A

Sieve Size (USS)	Sieve Size (mm)	% Passing
3.5"	87.50	100.0
3"	75.00	100.0
2"	50.00	100.0
1.5"	37.50	100.0
1"	25.00	100.0
3/4"	19.00	100.0
1/2"	12.50	100.0
3/8"	9.50	100.0
#4	4.75	100.0
#10	2.00	100.0
#20	0.850	100.0
#40	0.425	100.0
#60	0.250	100.0
#100	0.150	99.8
#200	0.075	95.6
-	0.0450	84.0
-	0.0321	82.1
-	0.0211	74.2
-	0.0129	60.3
-	0.0095	50.5
-	0.0068	44.5
-	0.0050	36.7
-	0.0036	30.7
-	0.0030	26.8
-	0.0015	18.3



** The test data given herein pertain to the sample provided only. This report constitutes a testing service only. Interpretation of the data can be provided upon request.*

TESTED BY	DATE	CHECKED BY	DATE
GP/JM/TM	March 31,2009	LP	March 31,2009

Golder Associates Ltd. - Burnaby Laboratory
4280 Still Creek Drive
Burnaby, B.C. Canada V5C 6C6

PARTICLE SIZE ANALYSIS OF SOILS

Reference
ASTM D 422-63 (2007)

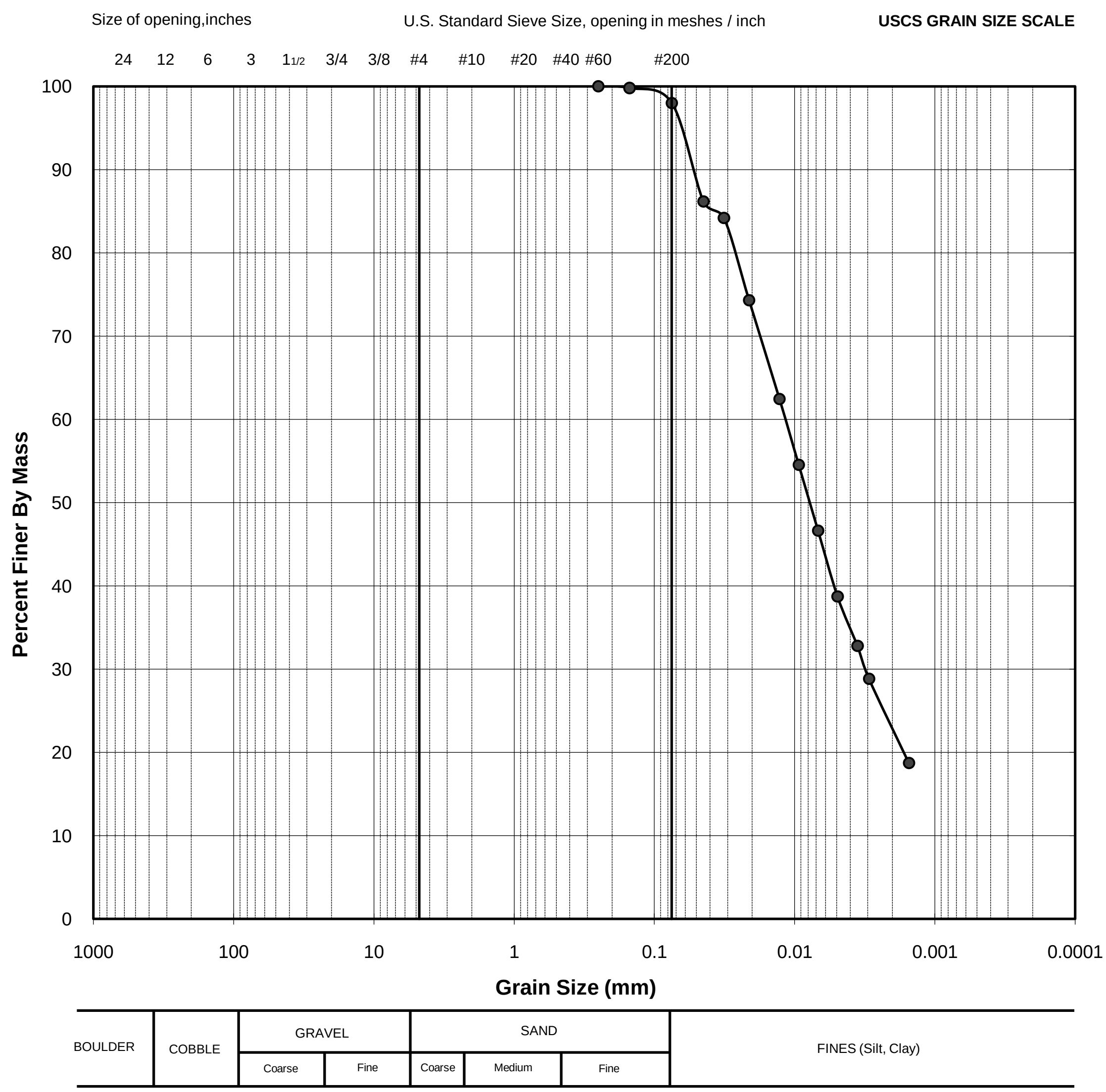
Project No.:	07-1416-0140	**Sample:**	**T2**
Client:	SGS Cemi Inc.	**Borehole No.:**	N/A
Project:	#0640	**Depth (m):**	N/A
Location:	Prize Mining Corp.	**Lab ID No:**	052

Specific Gravity (assumed): 2.70

Other Remarks:

Dispersion Method: Stirring
Dispersion Period (min): N/A

Sieve Size (USS)	Sieve Size (mm)	% Passing
3.5"	87.50	100.0
3"	75.00	100.0
2"	50.00	100.0
1.5"	37.50	100.0
1"	25.00	100.0
3/4"	19.00	100.0
1/2"	12.50	100.0
3/8"	9.50	100.0
#4	4.75	100.0
#10	2.00	100.0
#20	0.850	100.0
#40	0.425	100.0
#60	0.250	100.0
#100	0.150	99.8
#200	0.075	98.0
-	0.0446	86.2
-	0.0318	84.2
-	0.0211	74.3
-	0.0128	62.4
-	0.0093	54.5
-	0.0068	46.6
-	0.0049	38.7
-	0.0036	32.8
-	0.0029	28.8
-	0.0015	18.7



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TESTED BY	DATE	CHECKED BY	DATE
GP/JM/TM	March 31,2009	LP	March 31,2009

Golder Associates

Golder Associates Ltd. - Burnaby Laboratory
4280 Still Creek Drive
Burnaby, B.C. Canada V5C 6C6

PARTICLE SIZE ANALYSIS OF SOILS

Reference
ASTM D 422-63 (2007)

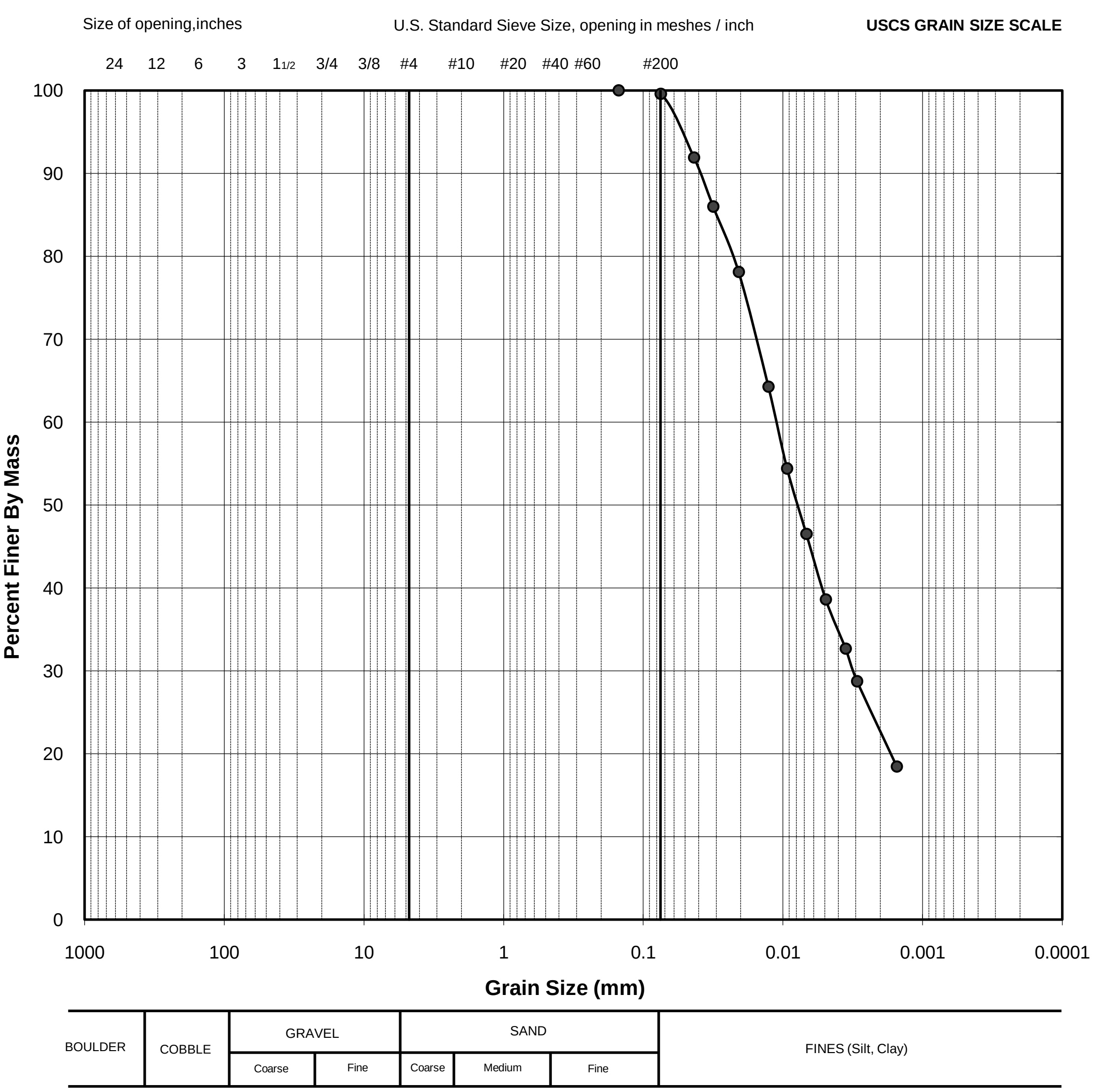
Project No.:	07-1416-0140	**Sample:**	**T3**
Client:	SGS Cemi Inc.	**Borehole No.:**	N/A
Project:	#0640	**Depth (m):**	N/A
Location:	Prize Mining Corp.	**Lab ID No:**	052

Specific Gravity (assumed): 2.70

Other Remarks:

Dispersion Method: Stirring
Dispersion Period (min): N/A

Sieve Size (USS)	Sieve Size (mm)	% Passing
3.5"	87.50	100.0
3"	75.00	100.0
2"	50.00	100.0
1.5"	37.50	100.0
1"	25.00	100.0
3/4"	19.00	100.0
1/2"	12.50	100.0
3/8"	9.50	100.0
#4	4.75	100.0
#10	2.00	100.0
#20	0.850	100.0
#40	0.425	100.0
#60	0.250	100.0
#100	0.150	100.0
#200	0.075	99.6
-	0.0433	91.9
-	0.0315	86.0
-	0.0207	78.1
-	0.0127	64.3
-	0.0093	54.4
-	0.0068	46.5
-	0.0049	38.6
-	0.0036	32.7
-	0.0029	28.8
-	0.0015	18.5



** The test data given herein pertain to the sample provided only. This report constitutes a testing service only. Interpretation of the data can be provided upon request.*

GP/JM/TM	March 31,2009	LP	March 31,2009
TESTED BY	DATE	CHECKED BY	DATE

CLIENT : Lorax
PROJECT : Prize Mining (Yellow Jacket Project)
CEMI Project # : 0640
TEST : Low-Level Metals by Aqua Regia Digestion with ICP-MS Finish
Date : April 2, 2009

Sample ID	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm
T1	0.42	39.45	3.93	37.1	998	818	46.4	770	4.02	39.5	0.8	2962.6	2.9	140.9	0.12	0.89	0.17	70
T2	0.45	37.36	4.1	38.7	318	777.9	44.5	755	4.03	39.6	0.9	530.2	3.7	152	0.13	0.91	0.17	69
T3	0.48	37.6	4.99	40.7	357	738.6	42	724	4	36.6	0.9	687.9	3.8	146.8	0.14	0.87	0.16	70

Sample ID	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Sc ppm	Tl ppm	S %	Hg ppb	Se ppm	Te ppm	Ga ppm
T1	2.92	0.118	17.7	479.8	7.02	81.1	0.011	<20	2.38	0.016	0.07	<0.1	10.4	0.02	<0.02	13	0.1	<0.02	6.6
T2	3.03	0.148	21.2	448.9	6.96	95.7	0.014	<20	2.33	0.018	0.07	<0.1	10.3	<0.02	<0.02	12	0.2	<0.02	6.6
T3	2.8	0.159	22.8	433.2	6.9	91.2	0.017	<20	2.35	0.018	0.07	<0.1	9.8	<0.02	<0.02	10	0.2	<0.02	6.6

TECHNICAL MEMORANDUM

To: **Bruce Graff P.Eng.; Chuck Downie, P.Geo.** **Date: April 27, 2009**
Linda Dandy, P.Geo

From: Andrew Rollo, P.Geo. **Project #: 489-2**

Subject: Preliminary Impact Assessment of Yellowjacket Process Plant Discharge on Pine Creek Water Quality

The objective of this technical memorandum is to provide a preliminary evaluation of the potential impacts to Pine Creek water quality resulting from the discharge of Yellowjacket process plant supernatant. The following discussion provides background upon which assumptions are based and results of the impact calculations conducted.

The Yellowjacket Gold Mine Project is located on Pine Creek near Atlin, in the northwestern corner of British Columbia. The geology hosting the gold mineralization is dominated by ultramafic and mafic rocks of the Atlin Ophiolitic Assemblage. Typical of ophiolitic assemblages, this package of rocks is composed of an imbricated sequence of oceanic crustal and upper mantle lithologies, including harzburgites, ultramafic cumulates, gabbros, diorites, and hypabyssal and extrusive basalts. Gold mineralization, which occurs in native form, is found to follow the strike of the Pine Creek fault. Previous geochemical characterization of Yellowjacket lithologies conducted in support of bulk sample permitting indicates that there is an abundance of carbonate neutralization potential (CaNP), with the majority of samples analyzed containing CaNP values greater than 100 kg $CaCO_3$/t (Lorax 2009). Additionally, acid potential (AP) of Yellowjacket lithologies is indicated to be very low, with a majority of samples containing sulphide sulphur concentrations at or below the detection limit (0.01%; Lorax 2009). Therefore, these data suggest that there is no potential for the generation of acid rock drainage (ARD) from Yellowjacket lithologies. Multi-element geochemistry data, obtained through aqua-regia digestion followed by ICP-MS, indicate that arsenic, cobalt, chromium, nickel, antimony, selenium, and thorium are elevated (greater than three times crustal abundance) in Yellowjacket Zone lithologies, suggesting that these elements may be of concern in drainage from waste produced from these materials (Lorax 2009a).

The current plans of the Atlin Gold Project involve the development of a series of pits, similar in dimensions to the bulk sample pit (70 m x 40 m), approximately 500 m eastward along the strike of the Pine Creek Fault (Figure 1-2). Development during

2009 will involve the extraction and processing of approximately 30,000 tonnes of material from the open pit. Ore will be processed using crushers and a Knelson Gravity concentrator, which uses centrifugal forces to separate the gold from the gangue materials. No chemicals are used in the processing of Yellowjacket ore, as the gold is in native form and does not require chemical treatment for extraction. Tailings generated from ore processing will be deposited, along with process plant discharge supernatant solution, to the tailings/sedimentation pond located within the alluvial gravels of the Pine Creek floodplain. Water from the tailings/sed pond will be allowed to exfiltrate to the groundwater within the alluvial gravels where it will eventually enter Pine Creek downstream. Currently, the Knelson concentrator at Yellowjacket is designed to process 150 m^3 of ore daily, which is equal to approximately 402 tonnes/day (2.68 t/m^3). The estimated volume of water that will be required to process Yellowjacket ore is 480 m^3/day. Therefore, the water-rock ratio in the process plant may be estimated to be approximately 1.2 m^3 of water per tonne of ore processed.

In order to evaluate the impact of the process plant discharge on the chemistry of Pine Creek, reasonable estimates of water quantity and quality are required. Table 1 provides a summary of the maximum flow rate expected from the Yellowjacket process plant as well as the flow conditions within Pine Creek, including low flow, average flow, and high flow. For the purposes of conducting a preliminary assessment of the impacts of Yellowjacket process plant discharge on Pine Creek water quality, it has been assumed that all effluent water from the process plant will discharge directly into Pine Creek. Based on this assumption, dilution factors, which have been calculated by dividing Pine Creek flow rates by the process plant discharge flow rate, are also reported in Table 1. These values demonstrate that even at winter low flow conditions, process plant effluent discharged directly to Pine Creek will be diluted a minimum of approximately 250 times. However, it is important to note that the low flow value included in Table 1 is from winter, when discharge from the process plant is not expected. Therefore, average and high flow dilution values provide a more reasonable estimation of the dilution expected within Pine Creek. While there is a good understanding of the quantity of water flowing from the process plant and within Pine Creek, there are no process plant water quality or kinetic leach experiment data currently available from the Yellowjacket Project to evaluate the quality of process plant discharge. Therefore, in the absence of site specific data, a reasonable approximation of Yellowjacket process plant discharge water chemistry is required.

Table 1:
Yellowjacket Process Plant and Pine Creek Flow Rates.

Source		Flow	Dilution Factor
Process Plant Discharge		0.0056 m^3/s	-
Pine Creek Flow[1]	Low	1.4 m^3/s	250
	Average	4.2 m^3/s	750
	High	14 m^3/s	2500

[1] Pine Creek Flow values from Sigma (2006)

The Ekati Mine, located approximately 300 km northeast of Yellowknife in the NWT, produces diamonds hosted within kimberlite pipes of the Lac de Gras Kimberlite field. Kimberlite is a mantle derived ultramafic volcanic rock that is composed predominantly of olivine and serpentine, both of which are common constituents of the mafic and ultramafic lithologies that dominate the Atlin Ophiolitic Complex where the Yellowjacket Property is located. Kimberlite Ore at Ekati is processed by crushing, washing, and gravity separation without the use of additional chemicals, very similar to the processing scheme that will be employed at Yellowjacket. It has been estimated that approximately 13,000 tonnes to 16,000 tonnes of ore are processed daily at Ekati (Day *et al*. 2003) using approximately 9,000 m^3 to 16,000 m^3 of water (Lee 2005), which produces water-rock ratios ranging from 0.7 m^3 water/ tonne up to 1 m^3 water/ tonne. The geology, ore processing scheme, and process plant water-rock ratios at Ekati are similar to those expected from the Yellowjacket project. Therefore, process plant discharge water quality from Ekati may serve as a reasonable approximation of process plant discharge expected from the Yellowjacket project.

Table 2 provides a summary of average process plant discharge water chemistry collected from Ekati between 2000 and 2002 (Rollo and Jamieson 2006). Note that only parameters with associated BC water quality objectives have been included in this analysis. This table also contains diluted Ekati process plant discharge concentrations, calculated by dividing the average process plant concentrations listed in Table 2 by the dilution factors listed in Table 1. Additionally, the detection limits that are currently being used for the 2009 Yellowjacket water quality monitoring program are included in this table for comparative purposes. For ease of comparison, the diluted concentrations reported in Table 2 have been formatted to the same number of decimal places as the detection limits. While these data demonstrate that the majority of trace metal concentrations in diluted process plant discharge waters are at or below the detection limits used in the 2009 water quality monitoring program, molybdenum and nickel are indicated to be present in detectable concentrations in diluted waters. However, comparison with baseline water quality data from Pine Creek (Lorax 2009b) demonstrates that the predicted concentrations for these parameters are at least an order of magnitude lower than the minimum baseline values.

As mentioned previously, Yellowjacket process plant effluent will not be discharged directly into Pine Creek; rather, it will be allowed to exfiltrate through the alluvial gravels of the Pine Creek floodplain. As a result of metal attenuation mechanisms within the alluvial gravel groundwater system, concentrations entering Pine Creek will most likely be less than those expected directly from the process plant. Therefore, these calculations, which provide a conservative overestimate of the potential impacts to Pine Creek, suggest that the discharge of Yellowjacket Process Plant effluent directly into Pine Creek will not have a significant impact on water quality

Table 2:
Average Process Plant Discharge water chemistry from Ekati Diamond Mine and Associated Dilution Calculations. Only parameters with BC water quality objectives have been included in this table. All values reported as mg/L unless specified otherwise.

	Average[1]	Diluted Concentration			2009 Detection Limit
		Low Flow[2]	Average Flow[3]	High Flow[4]	
SO_4	212	0.8	0.3	0.1	0.5
Cl	30.8	0.1	0.0	0.0	0.5
F	0.076	0.00	0.00	0.00	0.01
Ag	0.0002	0.000001	0.000000	0.000000	0.000005
Al	0.001	0.0000	0.0000	0.0000	0.0002
As	0.0126	0.00005	0.00002	0.00001	0.00002
B	0.0528	0.00	0.00	0.00	0.05
Cd	0.00066	0.000003	0.000001	0.000000	0.000005
Co	0.00051	0.000002	0.000001	0.000000	0.000005
Cr	0.00258	0.0000	0.0000	0.0000	0.0001
Cu	0.00156	0.00001	0.00000	0.00000	0.00005
Fe	0.046	0.000	0.000	0.000	0.001
Mn	0.0161	0.00006	0.00002	0.00001	0.00005
Mo	0.409	0.00164	0.00049	0.00016	0.00005
Ni	0.055	0.00022	0.00007	0.00002	0.00002
Pb	0.00006	0.000000	0.000000	0.000000	0.000005
Sb	0.02793	0.00011	0.00003	0.00001	0.00002
Se	0.00258	0.00001	0.00000	0.00000	0.00004
U	0.0002	0.000001	0.000000	0.000000	0.000002
V	0.0039	0.0000	0.0000	0.0000	0.0002
Zn	0.0042	0.0000	0.0000	0.0000	0.0001

[1] data from Rollo and Jamieson (2006)
[2] Dilution factor = 250 (Table 1)
[3] Dilution factor = 750 (Table 1)
[4] Dilution factor = 2500 (Table 1)
[5] reported as mg $CaCO_3$/L

References

Day, S., Sexsmith, K., and Millard, J. (2003). Acidic Drainage from Calcareous Coarse Kimberlite Reject, Ekati Diamond Mine, Northwest Territories, Canada. 6th International Conference on Acid Rock Drainage (ARD) 25 pp.

Lee, C.A. (2005). Evaluation of the Potential Use of Processed Kimberlite to Sequester CO2, Ekati Diamond Mine, NWT, Canada. M.Sc. Thesis, Queen's University, Kingston, Ontario.

Lorax (2009a). Yellowjacket Property Bulk Sample Waste Characterization Program. Prepared by Lorax Environmental Services for Prize Mining Corp. March 2009.

Lorax (2009b) Yellowjacket Gold Project – Baseline Water Quality Conditions (2006-2007 Monitoring). Prepared by Lorax Environmental Services for Prize Mining Corp. March 2009.

Rollo, H.A., and Jamieson, H.E. (2006). Interaction of Diamond Mine Waste and Surface Water in the Canadian Arctic. Applied Geochemistry 21, 1552 – 1538.

Sigma (2006). 2006 Atlin Hydroelectric Project, Hydrology Report. Prepared by Sigma Engineering Ltd for Taku Land Corporation.